

**PHASED ARRAY ANTENNA ABSORBER AND ASSOCIATED METHODS****Field of the Invention**

[0001] The present invention relates to the field of communications, and more particularly, to phased array antennas.

**Background of the Invention**

[0002] Existing microwave antennas include a wide variety of configurations for various applications, such as satellite reception, remote broadcasting, or military communication. The desirable characteristics of low cost, light weight, low profile and mass producibility are provided in general by printed circuit antennas. The simplest forms of printed circuit antennas are microstrip antennas wherein flat conductive elements, such as monopole or dipole antenna elements, are spaced from a single essentially continuous ground plane by a dielectric sheet of uniform thickness. An example of a microstrip antenna is disclosed in U.S. Patent No. 3,995,277 to Olyphant.

[0003] The antennas are designed in an array and may be used for communication systems such as identification

of friend/foe (IFF) systems, personal communication service (PCS) systems, satellite communication systems, and aerospace systems, which require such characteristics as low cost, light weight, low profile, and a low sidelobe. The bandwidth and directivity capabilities of such antennas, however, can be limiting for certain applications.

[0004] The use of electromagnetically coupled dipole antenna elements can increase bandwidth. Also, the use of an array of dipole antenna elements can improve directivity by providing a predetermined maximum scan angle.

[0005] However, utilizing an array of dipole antenna elements presents a dilemma. The maximum grating lobe free scan angle can be increased if the dipole antenna elements are spaced closer together, but a closer spacing can increase undesirable coupling between the elements, thereby degrading performance. This undesirable coupling changes rapidly as the frequency varies, making it difficult to maintain a wide bandwidth.

[0006] One approach for compensating the undesirable coupling between dipole antenna elements is disclosed in U.S. Patent No. 6,417,813 to Durham, which is incorporated herein by reference in its entirety and which is assigned to the current assignee of the present invention. The Durham patent discloses a wideband phased array antenna comprising an array of dipole antenna elements, with each dipole antenna element comprising a medial feed portion and a pair of legs extending outwardly therefrom.

[0007] In particular, adjacent legs of adjacent dipole

antenna elements include respective spaced apart end portions having predetermined shapes and relative positioning to provide increased capacitive coupling between the adjacent dipole antenna elements. The increased capacitive coupling counters the inherent inductance of the closely spaced dipole antenna elements, in such a manner as the frequency varies so that a wide bandwidth may be maintained.

[0008] Each phased array antenna has a desired frequency range, and the ground plane is typically spaced from the array of dipole antenna elements less than about one-half a wavelength of a highest desired frequency. When the frequency is in the GHz range, the separation between the array of dipole antenna elements and the ground plane is less than 0.20 inch at 30 GHz, for example. However, if the frequency of operation of the phased array antenna is in the MHz range, the separation between the array of dipole antenna elements and the ground plane increases to about 19 inches at 300 MHz, for example.

[0009] Fielding a phased array antenna with a relatively large separation between the ground plane and the array of dipole antenna elements becomes rather cumbersome because of its bulkiness. Inflatable or collapsible antennas are sometimes used because they are light in weight, easily portable and are easily deployed. For example, U.S. Patent No. 5,132,699 to Rupp et al. discloses an inflatable phased array antenna formed on one or more generally planar and vertically inclined panels.

[0010] Each panel has a continuous outer wall, a

continuous inner wall and a plurality of web partitions extending between the inner and outer walls to form a series of inflatable tubular members. The inner wall is covered with a conducting material so that it forms a ground plane, and a plurality of dipole antenna elements are affixed to the web partitions and spaced from the ground plane in a predetermined relationship so that the phased array antenna will operate at the desired frequency range.

[0011] As the frequency range decreases from the GHz range to the MHz range, the size of the phased array antenna increases. This presents a problem when a low radar cross section (RCS) mode is required. For example, the RCS of a ship having a phased array antenna operating in the MHz range would be adversely affected because of the increased size of the array.

[0012] An ideal antenna is inherently a low RCS structure. An antenna is a transducer whose function is to maximize power transfer from a propagating electromagnetic wave in free space to a receiver. Some antennas, of course, are intended to maximize power transfer from a transmitter to a propagating free space wave, but a basic principle of electromagnetics known as reciprocity insures that the same structure works both ways. Since the ideal antenna maximizes power transfer to the receiver, it minimizes power scattered back to a hypothetical radar, i.e., RCS.

[0013] Of course, actual antennas are non-ideal. Typically, the maximum power transfer condition is only satisfied for a limited range of frequencies and for a limited range of incident wave directions. Directional

selectivity is often a design goal for antennas, so that the maximum power transfer condition is only met for a small range of directions and power transfer is minimized for undesired directions. However, over its operating range a good antenna is an efficient absorber of incident energy. Therefore, a broadband antenna with broad angular coverage has the potential to be a radar absorptive material (RAM).

#### Summary of the Invention

[0014] In view of the foregoing background, it is therefore an object of the present invention to provide a phased array antenna that acts as a wideband absorber, and therefore supports a low RCS mode when required.

[0015] This and other objects, features, and advantages in accordance with the present invention are provided by a phased array antenna to be connected to a transceiver and comprising a substrate, and an array of dipole antenna elements on the substrate to be connected to the transceiver. Each dipole antenna element may comprise a medial feed portion, and a pair of legs extending outwardly therefrom. Each dipole antenna element may further comprise a load, and a switch connected thereto for selectively coupling the load to the medial feed portion so that the dipole antenna element selectively functions as an absorber for absorbing received signals while the load dissipates energy associated therewith.

[0016] The respective switches and loads allow the phased array antenna to operate as an absorber. For example, if a ship or platform deploying the phased array

antenna intends to maintain a low RCS, then the elements are selectively coupled to their respective loads for dissipating the energy associated with the received signals. When communications is required, the respective switches uncouple the loads so that the signals are passed along to the transmission and reception controller.

[0017] The phased array antenna may comprise an inflatable substrate with the array of dipole antenna elements thereon. An inflating device is used to inflate the substrate. The inflatable substrate addresses the deployment concerns of a large sized phased array antenna. When the phased array is not being deployed, or it is being transported, the inflatable substrate is deflated.

[0018] The inflating device may be an air pump, and when inflated, a dielectric layer of air is provided between the array of dipole antenna elements and the ground plane. At 300 MHz, for example, the thickness of the inflatable substrate is about 19 inches. Baffles or connections may extend between the two opposing sides of the inflatable substrate so that a uniform thickness is maintained by the substrate when inflated.

[0019] The respective switches and loads may be packaged within the inflatable substrate, or external the inflatable substrate. When the phased array antenna is to operate as an absorber, a controller switches the switches so that the loads are connected across the medial feed portions of the dipole antenna elements in the array.

[0020] An optional dielectric layer may be added

between the array of dipole antenna elements and the inflatable substrate. This dielectric layer preferably has a higher dielectric constant than the dielectric constant of the inflatable substrate when inflated. The higher dielectric constant helps to improve performance of the phased array antenna, particularly when the substrate is inflated with air, which has dielectric constant of 1. The inflatable substrate may be filled with a gas other than air. The inflatable substrate may comprise a polymer or an equivalent material for maintaining an enclosed flexible substrate when inflated.

[0021] In an alternate embodiment, the dipole antenna elements are permanently configured as an absorber by having a resistive element connected to the respective medial feed portions. Such an absorber may be used in an anechoic chamber, or may be placed adjacent to an object (e.g., a truck, a tank, etc.) to reduce its RCS, or may be even be placed on top of a building to reduce multipath interference from other signals. This absorber may be applicable to many other applications requiring a wideband absorber.

[0022] Another aspect of the present invention is directed to a method of making a phased array antenna that selectively functions as an absorber. The method comprises providing a substrate, and forming an array of dipole antenna elements on the substrate, with each dipole antenna element comprising a medial feed portion, and a pair of legs extending outwardly therefrom. Each dipole antenna element further comprises a passive load and a switch connected thereto for selectively coupling the passive load to the medial feed portion so that the

dipole antenna element selectively functions as an absorber for absorbing received signals while the passive load dissipates energy associated therewith.

#### Brief Description of the Drawings

[0023] FIG. 1 is a schematic diagram of a phased array antenna in accordance with the present invention mounted on a ship.

[0024] FIG. 2 is a schematic perspective view of the phased array antenna of FIG. 1 and a corresponding cavity mount.

[0025] FIG. 3 is an exploded view of the phased array antenna of FIG. 2.

[0026] FIG. 4 is a greatly enlarged view of a portion of the array of FIG. 2.

[0027] FIGS. 5A and 5B are enlarged schematic views of the spaced apart end portions of adjacent legs of adjacent dipole antenna elements as may be used in the phased array antenna of FIG. 2.

[0028] FIG. 5C is an enlarged schematic view of an impedance element electrically connected across the spaced apart end portions of adjacent legs of adjacent dipole antenna elements as may be used in the wideband phased array antenna of FIG. 2.

[0029] FIG. 5D is an enlarged schematic view of another embodiment of an impedance element electrically connected across the spaced apart end portions of adjacent legs of adjacent dipole antenna elements as may be used in the wideband phased array antenna of FIG. 2.

[0030] FIGS. 6A and 6B are enlarged schematic views of a discrete resistive element and a printed resistive



element connected across the medial feed portion of a dipole antenna element as may be used in the phased array antenna of FIG. 2.

[0031] FIGS. 7A and 7B are plots of computed VSWR versus frequency for an active dipole antenna element adjacent the edge elements in the phased array antenna of FIG. 2, and for the same active dipole antenna element without the edge elements in place.

[0032] FIGS. 8A and 8B are plots of computed VSWR versus frequency for an active dipole antenna element in the center of the phased array antenna of FIG. 2 with the edge elements in place, and for the same dipole antenna element without the edge elements in place.

[0033] FIG. 9 is a schematic diagram of a dipole antenna element having a switch and a load connected thereto so that the element selectively functions as an absorber in accordance with the present invention.

[0034] FIG. 10 is a cross-sectional diagram of a phased array antenna that includes the dipole antenna elements of FIG. 9.

[0035] FIG. 11 is top plan view of a building partly in sectional illustrating a feedthrough lens antenna in accordance with the present invention positioned in a wall of the building.

#### Detailed Description of the Preferred Embodiments

[0036] The present invention will now be described more fully hereinafter with reference to the accompanying drawings, in which preferred embodiments of the invention are shown. This invention may, however, be embodied in many different forms and should not be construed as

limited to the embodiments set forth herein. Rather, these embodiments are provided so that this disclosure will be thorough and complete, and will fully convey the scope of the invention to those skilled in the art. Like numbers refer to like elements throughout, and prime, double prime and triple prime notations are used to indicate similar elements in alternate embodiments.

[0037] Referring initially to FIGS. 1 and 2, a wideband phased array antenna 100 in accordance with the present invention will now be described. The phased array antenna 100 is particularly advantageous when design constraints limit the number of active dipole antenna elements in the array. The design constraints may be driven by a platform having limited installation space, and one which also requires a low radar cross section (RCS), such as the ship 112 illustrated in FIG. 1, for example. The illustrated phased array antenna 110 is connected to a transceiver and controller 114, as would be appreciated by those skilled in the art.

[0038] The phased array antenna 100 has edge elements 40b, and a corresponding cavity mount 200, as illustrated by the schematic perspective view in FIG. 2. The phased array antenna 100 comprises a substrate 104 having a first surface 106, and second surfaces 108 adjacent thereto and defining respective edges 110 therebetween. A plurality of dipole antenna elements 40a are on the first surface 106 and at least a portion of at least one dipole antenna element 40b is on one of the second surfaces 108. The dipole antenna elements 40b on the second surfaces 108 form the "edge elements" for the phased array antenna 100.

[0039] Normally, active and passive dipole antenna elements are on the same substrate surface. However, by separating the active and passive dipole antenna elements **40a**, **40b** onto two different substrate surfaces **106**, **108** having respective edges **110** defined therebetween, more space is available for the active dipole antenna elements. Consequently, antenna performance is improved for phased array antennas affected by design constraints.

[0040] In the illustrated embodiment, the second surfaces **108** are orthogonal to the first surface **106**. The substrate **104** has a generally rectangular shape having a top surface, and first and second pairs of opposing side surfaces adjacent the top surface and defining the respective edges **110** therebetween. The first surface **106** corresponds to the top surface, and the second surfaces **108** correspond to the first and second pairs of opposing side surfaces. The illustrated edge elements **40b** are on each of the pairs of opposing side surfaces. In different embodiments, the edge elements **40b** may be on just one of the pairs of opposing side surfaces, or even just one side surface. In addition, the substrate **104** is not limited to a rectangular shape, and is not limited to orthogonal side surfaces with respect to the top surface.

[0041] The edge elements **40b**, that is, the dipole antenna elements on the second surfaces **108**, may be completely formed on the second surfaces, or they may be formed so that part of these elements extend onto the first surface **106**. For the later embodiment, the substrate **104** may be a monolithic flexible substrate, and the second surfaces are formed by simply bending the

substrate so that one of the legs of the edge elements 40b extends onto the first surface 106. Alternatively, at least one of the legs of the dipole antenna elements 40a on the first surface 106 may extend onto the second surface 108.

[0042] The bend also defines the respective edges 110 between the first and second surfaces 106, 108. In lieu of a monolithic substrate, the first and second surfaces 106, 108 may be separately formed (with the respective dipole antenna elements 40a, 40b being formed completely on the respective surfaces 106, 108), and then joined together to form the substrate 104, as would be readily appreciated by those skilled in the art.

[0043] The illustrated phased array antenna 100 includes first and second sets of orthogonal dipole antenna elements to provide dual polarization. In alternate embodiments, the phased array antenna 100 may include only one set of dipole antenna elements.

[0044] The phased array antenna 100 is formed of a plurality of flexible layers, as shown in FIG. 3. As discussed above, the substrate 104, which is included within the plurality of flexible layers, may be a monolithic flexible substrate, and the second surfaces 108 are formed by simply bending the layers along the illustrated dashedline, for example. Excess material in the corners of the folded layers resulting from the second surfaces 108 being formed are removed, as would be appreciated by those skilled in the art.

[0045] The substrate 104 is sandwiched between a ground plane 30 and a cap layer 28. The substrate 104 is also known as a dipole layer or a current sheet, as would

be readily understood by those skilled in the art. Additionally, dielectric layers of foam 24 and an outer dielectric layer of foam 26 are provided. Respective adhesive layers 22 secure the substrate 104, ground plane 30, cap layer 28, and dielectric layers of foam 24, 26 together to form the phased array antenna 100. Of course, other ways of securing the layers may also be used as would be appreciated by those skilled in the art.

[0046] The dielectric layers 24, 26 may have tapered dielectric constants to improve the scan angle. For example, the dielectric layer 24 between the ground plane 30 and the dipole layer 20 may have a dielectric constant of 3.0, the dielectric layer 24 on the opposite side of the dipole layer 20 may have a dielectric constant of 1.7, and the outer dielectric layer 26 may have a dielectric constant of 1.2.

[0047] Referring now to FIGS. 4, 5A and 5B, the substrate 104 as used in the phased array antenna 100 will now be described in greater detail. The substrate 104 is a printed conductive layer having an array of dipole antenna elements 40 thereon, as shown in greater detail in the enlarged view of a portion 111 of the substrate 104. Each dipole antenna element 40 comprises a medial feed portion 42 and a pair of legs 44 extending outwardly therefrom. Respective feed lines would be connected to each feed portion 42 from the opposite side of the substrate 104.

[0048] Adjacent legs 44 of adjacent dipole antenna elements 40 have respective spaced apart end portions 46 to provide increased capacitive coupling between the adjacent dipole antenna elements. The adjacent dipole

antenna elements 40 have predetermined shapes and relative positioning to provide the increased capacitive coupling. For example, the capacitance between adjacent dipole antenna elements 40 is between about 0.016 and 0.636 picofarads (pF), and preferably between 0.159 and 0.239 pF. Of course, these values will vary as required depending on the actual application to achieve the same desired bandwidth, as readily understood by one skilled in the art.

[0049] As shown in FIG. 5A, the spaced apart end portions 46 in adjacent legs 44 may have overlapping or interdigitated portions 47, and each leg 44 comprises an elongated body portion 49, an enlarged width end portion 51 connected to an end of the elongated body portion, and a plurality of fingers 53, e.g., four, extending outwardly from the enlarged width end portion.

[0050] The adjacent legs 44 and respective spaced apart end portions 46 may have the following dimensions: the length E of the enlarged width end portion 51 equals 0.061 inches; the width F of the elongated body portions 49 equals 0.034 inches; the combined width G of adjacent enlarged width end portions 51 equals .044 inches; the combined length H of the adjacent legs 44 equals 0.276 inches; the width I of each of the plurality of fingers 53 equals 0.005 inches; and the spacing J between adjacent fingers 53 equals 0.003 inches.

[0051] The wideband phased array antenna 10 has a desired frequency range, e.g., 2 GHz to 30 GHz, and the spacing between the end portions 46 of adjacent legs 44 is less than about one-half a wavelength of a highest desired frequency. Depending on the actual application,

the desired frequency may be a portion of this range, such as 2 GHz TO 18 GHz, for example.

[0052] Alternatively, as shown in FIG. 5B, adjacent legs 44' of adjacent dipole antenna elements 40 may have respective spaced apart end portions 46' to provide increased capacitive coupling between the adjacent dipole antenna elements. In this embodiment, the spaced apart end portions 46' in adjacent legs 44' comprise enlarged width end portions 51' connected to an end of the elongated body portion 49' to provide the increased capacitive coupling between adjacent dipole antenna elements 40. Here, for example, the distance K between the spaced apart end portions 46' is about 0.003 inches.

[0053] To further increase the capacitive coupling between adjacent dipole antenna elements 40, a respective discrete or bulk impedance element 70" is electrically connected across the spaced apart end portions 46" of adjacent legs 44" of adjacent dipole antenna elements, as illustrated in FIG. 5C.

[0054] In the illustrated embodiment, the spaced apart end portions 46" have the same width as the elongated body portions 49". The discrete impedance elements 70" are preferably soldered in place after the dipole antenna elements 40 have been formed so that they overlay the respective adjacent legs 44" of adjacent dipole antenna elements 40. This advantageously allows the same capacitance to be provided in a smaller area, which helps to lower the operating frequency of the wideband phased array antenna 10.

[0055] The illustrated discrete impedance element 70" includes a capacitor 72" and an inductor 74" connected

together in series. However, other configurations of the capacitor 72" and inductor 74" are possible, as would be readily appreciated by those skilled in the art. For example, the capacitor 72" and inductor 74" may be connected together in parallel, or the discrete impedance element 70" may include the capacitor without the inductor or the inductor without the capacitor.

Depending on the intended application, the discrete impedance element 70" may even include a resistor.

[0056] The discrete impedance element 70" may also be connected between the adjacent legs 44 with the overlapping or interdigitated portions 47 illustrated in FIG. 5A. In this configuration, the discrete impedance element 70" advantageously provides a lower cross polarization in the antenna patterns by eliminating asymmetric currents which flow in the interdigitated capacitor portions 47. Likewise, the discrete impedance element 70" may also be connected between the adjacent legs 44' with the enlarged width end portions 51' illustrated in FIG. 5B.

[0057] Another advantage of the respective discrete impedance elements 70" is that they may have different impedance values so that the bandwidth of the wideband phased array antenna 10 can be tuned for different applications, as would be readily appreciated by those skilled in the art. In addition, the impedance is not dependent on the impedance properties of the adjacent dielectric layers 24 and adhesives 22. Since the discrete impedance elements 70" are not effected by the dielectric layers 24, this approach advantageously allows the impedance between the dielectric layers 24 and the



impedance of the discrete impedance element 70" to be decoupled from one another.

[0058] Yet another approach to further increase the capacitive coupling between adjacent dipole antenna elements 40 includes placing a respective printed impedance element 80"" adjacent the spaced apart end portions 46"" of adjacent legs 44"" of adjacent dipole antenna elements 40, as illustrated in FIG. 5D.

[0059] The respective printed impedance elements 80"" are separated from the adjacent legs 44"" by a dielectric layer, and are preferably formed before the dipole antenna layer 20 is formed so that they underlie the adjacent legs 44"" of the adjacent dipole antenna elements 40. Alternatively, the respective printed impedance elements 80"" may be formed after the dipole antenna layer 20 has been formed. For a more detailed explanation of the printed impedance elements, reference is directed to U.S. Patent Application Serial No. 10/308,424 which is assigned to the current assignee of the present invention, and which is incorporated herein by reference.

[0060] A respective load 150 is preferably connected to the medial feed portions 42 of the dipole antenna elements 40d on the second surfaces 108 so that they will operate as dummy dipole antenna elements. The load 150 may include a discrete resistor, as illustrated in FIG. 6A, or a printed resistive element 152, as illustrated in FIG. 6B. Each discrete resistor 150 is soldered in place after the dipole antenna elements 40d have been formed. Alternatively, each discrete resistor 150 may be formed by depositing a resistive paste on the medial feed

portions 42, as would be readily appreciated by those skilled in the art. The respective printed resistive elements 152 may be printed before, during or after formation of the dipole antenna elements 40d, as would also be readily appreciated by those skilled in the art. The resistance of the load 150 is typically selected to match the impedance of a feed line connected to an active dipole antenna element, which is in a range of about 50 to 100 ohms.

[0061] A ground plane 30 is adjacent the plurality of dipole antenna elements 40a, 40b, and to further improve performance of the phased array antenna 100, the edge elements 40b are electrically connected to the ground plane. The ground plane 30 is preferably spaced from the first surface 106 of the substrate 104 less than about one-half a wavelength of a highest desired frequency.

[0062] For an array of 18 active dipole antenna elements on the first surface 106 of the substrate 104, FIG. 7A is a plot of computed VSWR versus frequency for the active dipole antenna element immediately adjacent the edge elements 40b, and FIG. 7B is also a plot of computed VSWR versus frequency for the same active dipole antenna element except without the edge elements in place. Line 160 illustrates that there is advantageously a low VSWR between 0.10 and 0.50 GHz with the edge elements 40b in place. The edge elements 40b allow the immediately adjacent active dipole antenna elements to receive sufficient current, which is normally conducted through the dipole antenna elements 40a, 40b on the substrate 104.

[0063] Referring now to FIGS. 8A and 8B, the VSWR versus frequency remains fairly the same between the two configurations (i.e., with and without the edge elements 40b in place) with respect to the active dipole antenna elements 40a in or near the center of the first surface 106. Line 164 illustrates the computed VSWR for an active dipole antenna element with the edge elements 40b in place, and line 166 illustrates the computed VSWR for the same active dipole antenna element without the dummy elements in place.

[0064] In the illustrated phased array antenna 100, there are 18 dipole antenna elements 40a on the first surface 106 and 18 dipole antenna elements 40b on the second surfaces 108. Even though the number of dipole antenna elements for this type of phased array antenna 100 is not limited to any certain number of elements, it is particularly advantageous when the number of elements is such that the percentage of edge elements 40b on the second surfaces 108 is large when compared to the percentage of active dipole antenna elements 40a on the first surface 106. Performance of the phased array antenna 100 is improved because the active elements 40a extend to the edges 110 of the first surface 106 of the substrate 104.

[0065] The corresponding cavity mount 200 for the phased array antenna 100 with edge elements 40d will now be discussed in greater detail. The cavity mount 200 is a box having an opening therein for receiving the phased array antenna 100, and comprises a signal absorbing surface 204 adjacent each second surface 108 of the substrate 104 having edge elements 40b thereon.

[0066] As discussed above, the dipole antenna elements **40b** on the second surfaces **108** are dummy elements. Even though the dummy elements **40b** are not connected to a feed line, they still receive signals at the respective loads **150** connected across the medial feed portions **42**. To prevent these signals from being reflected within the cavity mount **200**, the signal absorbing surfaces **204** are placed adjacent the dummy elements **40b**.

[0067] Without the signal absorbing surfaces **204** in place, the reflected signals would create electromagnetic interference (EMI) problems, and they may also interfere with the adjacent active dipole antenna elements **40a** on the first surface **106** of the substrate **104**. The signal absorbing surfaces **204** thus absorb reflected signals so that the dipole antenna elements **40a** on the first surface **106** appear as if they are in a free space environment.

[0068] Each signal absorbing surface **204** comprises a ferrite material layer **204a** and a conducting layer **204b** adjacent thereto. The conducting layer **204b**, such as a metal layer, prevents any RF signals from radiating external the cavity mount **200**. Instead of a ferrite material layer, another type of RF absorbing material layer may be used, as would be readily appreciated by one skilled in the art.

[0069] In alternate embodiments, the signal absorbing surfaces **204** include a resistive layer and a conductive layer thereto. The resistive layer is coated on the conductive layer so that the conductive layer functions as a signal absorbing surface. The embodiment of the signal absorbing surfaces does not include the ferrite material layer **204a**, which reduces the weight of the

cavity mount 200. In yet another alternate embodiment, the signal absorbing surfaces 204 includes just the conductive layer.

[0070] When the phased array antenna 100 is positioned within the cavity mount 200, the first surface 106 of the substrate 104 is substantially coplanar with an upper surface of the cavity mount. The height of the ferrite material layer 204a is preferably at least equal to a height of the second surface 108 of the substrate 104. In addition, the cavity mount 200 also carries a plurality of power dividers 208 for interfacing with the dipole antenna elements 40a on the first surface 106 of the substrate 104. When the second surface 108 is orthogonal to the first surface 106 of the substrate 104, the cavity mount 200 has a bottom surface 206 that is also orthogonal to the signal absorbing surfaces 204.

[0071] Yet another aspect of the present invention is directed to a phased array antenna 300 that selectively functions as an absorber. In particular, each dipole antenna element 40 has a switch 302 connected to its medial feed portion 42 via feed lines 303, and a passive load 304 is connected to the switch, as illustrated in FIG. 9. The switch 302, in response to a control signal generated by a switch controller 307, selectively couples the passive load 304 to the medial feed portion 42 so that the dipole antenna element 40 selectively functions as an absorber for absorbing received signals.

[0072] The passive load 304 is sized to dissipate the energy associated with the received signal, and may comprise a printed resistive element or a discrete resistor, as would be readily appreciated by those

skilled in the art. For example, the resistance of the passive load 304 is typically between 50 to 100 ohms to match the impedance of the feed lines 303 when the dipole antenna element 40 passes along the received signals for processing.

[0073] As the frequency range decreases from the GHz range to the MHz range, the size of the phased array antenna significantly increases. This presents concerns when a low radar cross section (RCS) mode is required, and also in terms of deployment because of the increased size of the phased array antenna.

[0074] With respect to the RCS concerns, the respective switches 302 and passive loads 304 allow the phased array antenna 300 to operate as an absorber. For example, if a ship or any other type platform (fixed or mobile) deploying the phased array antenna 300 intends to maintain a low RCS, then the elements are selectively coupled to their respective passive loads 304 for dissipating the energy associated with any received signals. When communications is required, the respective switches 306 uncouple the passive loads 304 so that the signals are passed along to the transmission and reception controller 14.

[0075] Each phased array antenna has a desired frequency range, and the ground plane 310 is typically spaced from the array of dipole antenna elements 40 less than about one-half a wavelength of a highest desired frequency. In addition, the dipole antenna elements 40 may also be spaced apart from one another less than about one-half a wavelength of the highest desired frequency.

[0076] When the frequency is in the GHz range, the separation between the array of dipole antenna elements 40 and the ground plane 310 is less than 0.20 inch at 30 GHz, for example. This does not necessarily present a problem in terms of RCS and deployment. However, when the frequency of operation of the phased array antenna 300 is in the MHz range, the separation between the array of dipole antenna elements 40 and the ground plane 310 increases to about 19 inches at 300 MHz, for example. This is where the RCS and deployment concerns arise because of the increased dimensions of the phased array antenna 300.

[0077] Referring now to FIG. 10, the illustrated phased array antenna 300 comprises an inflatable substrate 306 with the array of dipole antenna elements 40 thereon. An inflating device 308 is used to inflate the substrate 306. The inflatable substrate 306 addresses the deployment concerns. When the phased array 300 is not being deployed, or it is being transported, the inflatable substrate 306 is deflated. However, once the phased array antenna 300 is in the field and is ready to be deployed, the inflatable substrate 306 is inflated.

[0078] The inflating device 308 may be an air pump, and when inflated, a dielectric layer of air is provided between the array of dipole antenna elements 40 and the ground plane 310. At 300 MHz, the thickness of the inflatable substrate 306 is about 19 inches. Baffles or connections 312 may extend between the two opposing sides of the inflatable substrate 306 so that a uniform thickness is maintained by the substrate when inflated,

as would be readily appreciated by those skilled in the art.

[0079] The respective switches 302 and loads 304 may also be packaged within the inflatable substrate 306. Consequently, the corresponding feed lines 303 and control lines also pass through the inflatable substrate 306. In alternate embodiments, the respective switches 302 and loads 304 may be packaged external the inflatable substrate 306. When the phased array antenna 300 is to operate as an absorber, the controller 307 switches the switches 302 so that the loads 304 are connected across the medial feed portions 42 of the dipole antenna elements 40 in the array.

[0080] An optional dielectric layer 320 may be added between the array of dipole antenna elements 40 and the inflatable substrate 306. The dielectric layer 320 preferably has a higher dielectric constant than the dielectric constant of the inflatable substrate 306 when inflated. The higher dielectric constant helps to improve performance of the phased array antenna 300, particularly when the substrate 306 is inflated with air, which has dielectric constant of 1. The dielectric layer 320 would have a dielectric constant that is greater than 1, and preferably within a range of about 1.2 to 3, for example. The inflatable substrate 306 may be filled with a gas other than air, as would be readily appreciated by those skilled in the art, in which case the dielectric layer 320 may not be required. The inflatable substrate 306 may even be inflated with a curable material.

[0081] The inflatable substrate 306 preferably comprises a polymer. However, other materials for



maintaining an enclosed flexible substrate may be used, as would be readily appreciated by those skilled in the art. The array of dipole antenna elements 40 may be formed directly on the inflatable substrate 306, or the array may be formed separately and attached to the substrate with an adhesive. Similarly, the ground plane 310 may be formed as part of the inflatable substrate 306, or it may be formed separately and is also attached to the substrate with an adhesive.

[0082] In an alternative embodiment of the phased array antenna 300, the dipole antenna elements 40 are permanently configured as an absorber by having a resistive element connected to the respective medial feed portions 42, as illustrated in FIGS. 6A and 6B. Such an absorber may be used in an anechoic chamber, or may be placed adjacent an object (e.g., a truck, a tank, etc.) to reduce its RCS, or may be even be placed on top of a building to reduce multipath interference from other signals.

[0083] As discussed above, another aspect of the present invention is to further increase the capacitive coupling between adjacent dipole antenna elements 40 using an impedance element 70" or 80"" electrically connected across the spaced apart end portions 46", 46"" of adjacent legs 44" of adjacent dipole antenna elements, as illustrated in FIG. 5C and 5D. This aspect of the present invention is not limited to the phased array antenna 100 illustrated above. In other words, the impedance elements 70", 80"" may be used on larger size substrate 104, as discussed in U.S. Patent No. 6,512,487

to Taylor et al., which has been incorporated herein by reference.

[0084] For example, the substrate may be twelve inches by eighteen inches. In this example, the number of dipole antenna elements 40 correspond to an array of 43 antenna elements by 65 antenna elements, resulting in an array of 2795 dipole antenna elements.

[0085] For this larger size substrate, the array of dipole antenna elements 40 may be arranged at a density in a range of about 100 to 900 per square foot. The array of dipole antenna elements 40 are sized and relatively positioned so that the phased array antenna is operable over a frequency range of about 2 to 30 GHz, and at a scan angle of about  $\pm 60$  degrees (low scan loss). Such an antenna 100' may also have a 10:1 or greater bandwidth, includes conformal surface mounting (on an aircraft, for example), while being relatively light weight, and easy to manufacture at a low cost. As would be readily appreciated by those skilled in the art, the array of dipole antenna elements 40 in accordance with the present invention may be sized and relatively positioned so that the wideband phased array antenna is operable over other frequency ranges, such as in the MHz range, for example.

[0086] Referring now to FIG. 11, yet another aspect of the present invention is directed to a feedthrough lens antenna 60 that includes this larger size substrate. The feedthrough lens antenna 60 includes first and second phased array antennas 100a', 100b', which are preferably substantially identical. For a more detailed explanation on the feedthrough lens antenna 60, reference is directed

to U.S. Patent No. 6,417,813 to Durham, which is incorporated herein by reference in its entirety and which is assigned to the current assignee of the present invention.

[0087] The feedthrough lens antennas may be used in a variety of applications where it is desired to replicate an electromagnetic (EM) environment within a structure, such as a building 62, over a particular bandwidth. For example, the feedthrough lens antenna 60 may be positioned on a wall 61 of the building 62. The feedthrough lens antenna 60 allows EM signals 63 from a transmitter 80 (e.g., a cellular telephone base station) to be replicated on the interior of the building 62 and received by a receiver 81 (e.g., a cellular telephone). Otherwise, a similar signal 64 may be partially or completely reflected by the walls 61.

[0088] The first and second phased array antennas 100a', 100b' are connected by a coupling structure 66 in a back-to-back relation. The first and second phased array antennas 100a', 100b are substantially similar to the antenna 100 described above, except with the edge elements 40b preferably removed.

[0089] In addition, other features relating to the phased array antennas are disclosed in copending patent applications filed concurrently herewith and assigned to the assignee of the present invention and are entitled PHASED ARRAY ANTENNA WITH EDGE ELEMENTS AND ASSOCIATED METHODS, attorney docket number 51308; CAVITY MOUNT FOR PHASED ARRAY ANTENNA WITH EDGE ELEMENTS AND ASSOCIATED METHODS, attorney docket number 51312; METHOD FOR DEPLOYING A PHASED ARRAY ANTENNA ABSORBER, attorney

docket number, 51321; and PHASED ARRAY ANTENNA WITH DISCRETE CAPACITIVE COUPLING AND ASSOCIATED METHODS, attorney docket number 51309, the entire disclosures of which are incorporated herein in their entirety by reference.

[0090] Many modifications and other embodiments of the invention will come to the mind of one skilled in the art having the benefit of the teachings presented in the foregoing descriptions and the associated drawings. Therefore, it is understood that the invention is not to be limited to the specific embodiments disclosed, and that modifications and embodiments are intended to be included within the scope of the appended claims.